

# Determining Real Permittivity from Fresnel Coefficients in GNSS-R

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**Abstract**—Global Navigation Satellite System Reflectometry (GNSS-R) can be used to derive information about the composition or the properties of ground surfaces, by analyzing signals emitted by GNSS satellites and reflected from the ground. If the received power is measured with linearly polarized antennas, under the condition of smooth surface, the reflected signal is proportional to the modulus of the perpendicular and parallel polarization Fresnel coefficients, which depend on the incidence angle  $\theta$ , and on the dielectric constant  $\varepsilon$  of the soil. In general,  $\varepsilon$  is a complex number; for non-dispersive soils, the imaginary part of  $\varepsilon$  can be neglected, and a real value of  $\varepsilon$  is sought. We solve the real-valued problem explicitly giving formulas that can be used to determine the dielectric constant  $\varepsilon$  and we compare the analytical solution with experimental data in the case of sand soil.

## 1. INTRODUCTION

Global Navigation Satellite System Reflectometry (GNSS-R) is a technique for sensing the Earth surface, based on the principle of detecting GNSS signals reflected off the ground, and processing them to monitor its properties remotely (see [1]). This application is a key input in the areas of ocean observation (see e.g., [2]), ice (see e.g., [3, 4]) and land remote sensing (see e.g., [5–7]), altimetry (see e.g., [8, 9]), climate modeling and weather prediction [10]. The passive bi-static radar configuration used in this technique requires no transmitters except GNSS satellites, thus enabling the system to be light and compact (see e.g., [11–14]). The Signal to Noise (SNR) data recorded by GNSS receivers are related to the direct signals and those reflected by the ground. Under the assumption that the surface be flat, and considering a receiving antenna either vertically or horizontally polarized, the SNR is related to the Fresnel reflection coefficients for vertical and horizontal polarization, which are functions of the relative permittivity of the soil and of the incident angle [15]. The relative permittivity of the soil is generally obtained by solving the Fresnel coefficient equations numerically; then, the soil moisture can be obtained by applying several well established models (see for example the semi-empirical models of [16, 17]). These models may be useful for the monitoring of a field of known characteristics in terms of sand, clay percentage, etc. In more general cases, i.e., for non-flat surfaces, more powerful techniques of inverse scattering should be used [18].

## 2. STATEMENT OF THE PROBLEM

The total electromagnetic field received by the down-looking antenna is the sum of various signals, scattered by the Earth's surface (see Fig. 1). These are essentially of two kinds: coherent and incoherent [19]. If the surface is approximately smooth, the non-coherent component is negligible, and the total power received by the antenna can be approximated by the coherent part only [5].

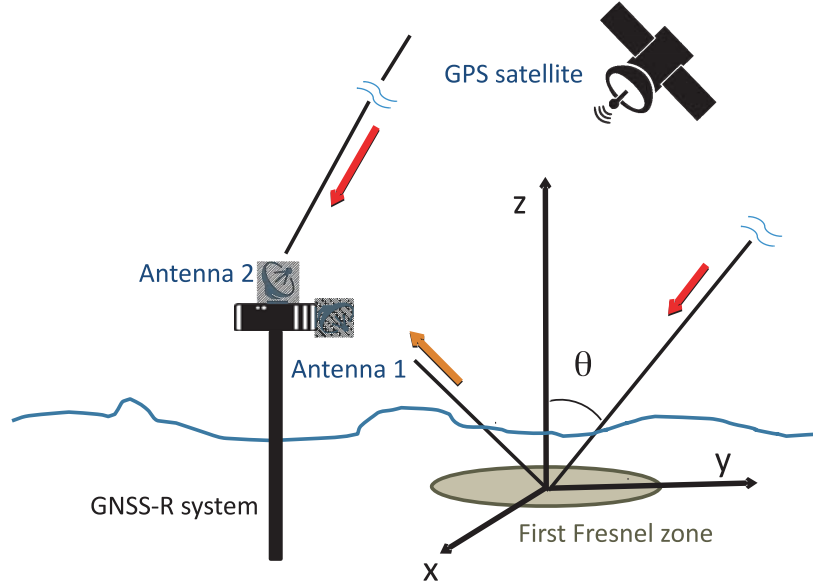
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**Figure 1.** GNSS reflectometry geometry.

The coherent component in the GPS bistatic radar is given by

$$P_{pol,coh} = R_{pol} \frac{P_t G_t G_r \lambda^2}{(4\pi)^2 (r_1 + r_2)^2}, \quad (1)$$

where the product  $P_t G_t$  is the Equivalent Isotropic Radiated Power (EIRP) of the transmitted signal;  $G_r$  is the receiver antenna gain;  $\lambda$  is the wavelength ( $\lambda = 19.042$  cm for GPS L1 signal);  $r_1$  and  $r_2$  are, respectively, the distance between the receiver and the specular point, and that between the specular point and satellite;  $R_p$  is the power reflectivity of the reflecting surface at a specified polarization ( $pol$ ). For smooth surfaces, the reflectivity can be approximated by

$$R_{pol} = |\Gamma_{pol}|^2, \quad (2)$$

where  $\Gamma_{pol}$  is the Fresnel reflection coefficient. In the case of perpendicular (or horizontal, or TE) polarization and parallel (or vertical, or TM) polarization, the corresponding Fresnel reflection coefficients can be written, respectively, as:

$$\Gamma_n = \frac{\cos \theta - \sqrt{\varepsilon - \sin^2 \theta}}{\cos \theta + \sqrt{\varepsilon - \sin^2 \theta}}, \quad \Gamma_p = \frac{\varepsilon \cos \theta - \sqrt{\varepsilon - \sin^2 \theta}}{\varepsilon \cos \theta + \sqrt{\varepsilon - \sin^2 \theta}}. \quad (3)$$

As mentioned in [20], our goal is to find the value of the permittivity  $\varepsilon$  from these two relations. For general media, including in particular dispersive ones,  $\varepsilon$  is a complex number and can be found from Equation (3), interpreted as a system of two equations in the two unknowns  $\Re(\varepsilon)$  and  $\Im(\varepsilon)$ . For non-dispersive media,  $\varepsilon$  is a real number, and can be found from either of the two relations in Eq. (3), which can be solved individually, and explicitly, for real  $\varepsilon$ . Thus, one can choose to carry out the measurements relative to either the perpendicular or the parallel case. As we show, the first equation of Eq. (3) (i.e., the perpendicular case) is much simpler to solve; on the other hand, the measurements of  $\Gamma_p$  may point to the evidence of the so-called Brewster angle  $\theta_B$ , in which case the determination of  $\varepsilon$  is immediate. While the simplest expression  $\varepsilon_p = \tan^2 \theta_B$  is well known, it is in practice quite difficult if not impossible to use it; hence, the merit of alternative formulas such as the ones we describe here. At any rate, one needs to be sure that the value of  $\varepsilon$  determined by either equation is the same, and also independent of the particular value of  $\theta$  at which the measurement is taken; this can happen only if the angle and the coefficients satisfy a mutual compatibility condition, which can also be described (and, therefore, checked) explicitly. In the sequel, we clarify these remarks in the particular situation in which we have measurements of the moduli  $\gamma_n = |\Gamma_n|$  and  $\gamma_p = |\Gamma_p|$ , as per Eq. (2). We provide explicit, real solutions to Eq. (3), and compare our results with those of [18] for dry sand. This method can be generalized to equations of similar kind.

### 3. THE FRESNEL INVERSE PROBLEM

We look for real solutions  $\varepsilon > 1$  (to signify that the medium is denser than air) to either the equation

$$\left| \frac{\cos \theta - \sqrt{\varepsilon - \sin^2 \theta}}{\cos \theta + \sqrt{\varepsilon - \sin^2 \theta}} \right| = |\Gamma_n| =: \gamma_n, \tag{4}$$

or

$$\left| \frac{\varepsilon \cos \theta - \sqrt{\varepsilon - \sin^2 \theta}}{\varepsilon \cos \theta + \sqrt{\varepsilon - \sin^2 \theta}} \right| = |\Gamma_p| =: \gamma_p, \tag{5}$$

with  $\theta \in [0, \frac{\pi}{2}[$  and, correspondingly,  $0 < \gamma_p \leq \gamma_n < 1$  (these conditions are necessarily satisfied if Eqs. (4) and (5) do have a common solution). Then, Equation (4) has a unique solution  $\varepsilon_n > 1$ , given by

$$\varepsilon_n = 1 + \frac{4\gamma_n \cos^2 \theta}{(1 - \gamma_n)^2}. \tag{6}$$

This solution is constant under certain compatibility conditions between  $\gamma_n$  and  $\theta$  similar to Eq. (15), in the sense that  $\varepsilon$  is independent of the particular angle  $\theta$  at which the values of  $\gamma_n$  is measured. The determination of an explicit, constant solution of Eq. (5) is more complicated. We assume that there is  $\theta_B \in ]\frac{\pi}{4}, \frac{\pi}{2}[$ , corresponding to which  $\gamma_p = 0$  ( $\theta_B$  is the Brewster angle; this too is a necessary condition for solvability). We define

$$\lambda_p := \frac{1 + \gamma_p}{1 - \gamma_p} \geq 1, \tag{7}$$

and note that  $\lambda_p = 1$  only when  $\gamma_p = 0$ . We define further

$$\mu_p := \begin{cases} \lambda_p & \text{if } 0 \leq \theta \leq \theta_B, \\ \frac{1}{\lambda_p} & \text{if } \theta_B \leq \theta < \frac{\pi}{2} \end{cases} \tag{8}$$

(recall that  $\lambda_p = \frac{1}{\lambda_p} = 1$  at  $\theta_B$ ), and

$$\theta_1 := \begin{cases} \frac{\pi}{2} & \text{if } \tan^2 \theta_B \geq 2, \\ \arcsin \left( \frac{1}{\sqrt{2}} \tan \theta_B \right) & \text{if } \tan^2 \theta_B < 2. \end{cases} \tag{9}$$

Then, Equation (5) has a solution  $\varepsilon_p > 1$ , given by

$$\varepsilon_p = \frac{\mu_p}{2 \cos^2 \theta} \left( \mu_p + \operatorname{sgn}(\theta_1 - \theta) \sqrt{\mu_p^2 - \sin^2(2\theta)} \right). \tag{10}$$

This solution is obtained by patching together three different solutions  $\varepsilon_p^0$ , defined on all of  $[0, \frac{\pi}{2}[$ , and  $\varepsilon_p^1, \varepsilon_p^2$ , defined only in  $[\theta_B, \frac{\pi}{2}[$ , as long as  $\lambda_p \sin(2\theta) \leq 1$  in this interval. The three solutions are given by:

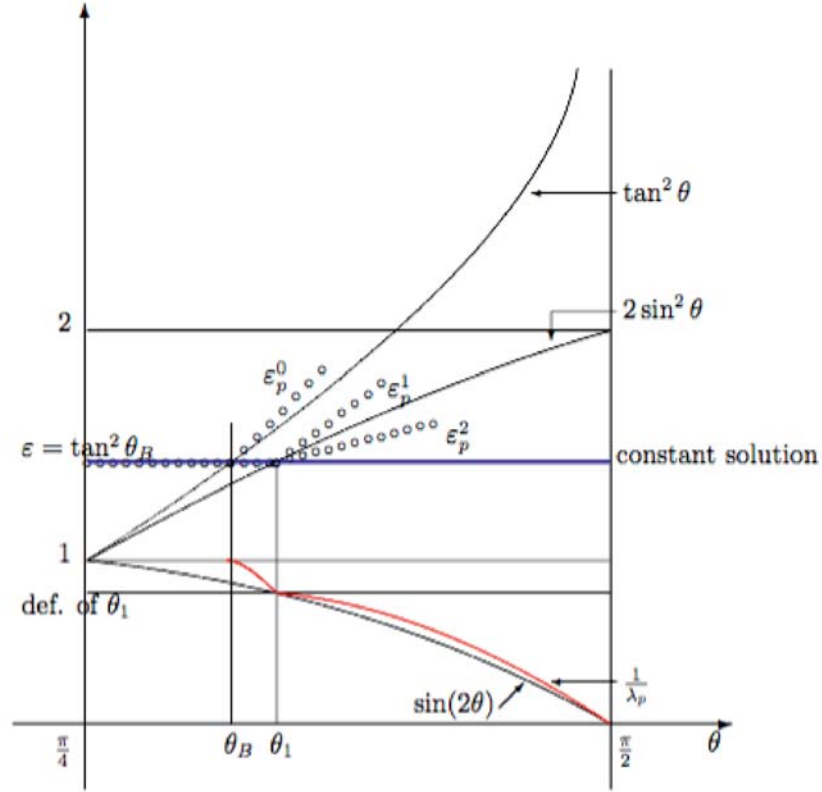
$$\varepsilon_p^0 = \frac{\lambda_p^2}{2 \cos^2 \theta} \left( 1 + \sqrt{1 - \frac{\sin^2(2\theta)}{\lambda_p^2}} \right), \tag{11}$$

$$\varepsilon_p^1 = \frac{1}{2\lambda_p^2 \cos^2 \theta} \left( 1 + \sqrt{1 - \lambda_p^2 \sin^2(2\theta)} \right), \tag{12}$$

$$\varepsilon_p^2 = \frac{1}{2\lambda_p^2 \cos^2 \theta} \left( 1 - \sqrt{1 - \lambda_p^2 \sin^2(2\theta)} \right). \tag{13}$$

In principle, these solutions depend on  $\theta$ , and satisfy the conditions:

$$\varepsilon_p^0 \geq \tan^2 \theta \geq \varepsilon_p^1 \geq 2 \sin^2 \theta \geq \varepsilon_p^2 \geq 1. \tag{14}$$



**Figure 2.** Solution of (5). On  $[\frac{\pi}{4}, \theta_B]$ ,  $\varepsilon = \tan^2 \theta_B = \varepsilon_p^0$ ; on  $[\theta_B, \theta_1]$ ,  $\varepsilon = \tan^2 \theta_B = \varepsilon_p^1$ ; on  $[\theta_1, \frac{\pi}{2}]$ ,  $\varepsilon = \tan^2 \theta_B = \varepsilon_p^2$ .

We find that the constant solution to the Fresnel formulas is given by  $\varepsilon_p = \tan^2 \theta_B$  (as is well known); however,  $\varepsilon_p^0$  can be constant only if  $\theta$  varies between  $\frac{\pi}{4}$  and  $\theta_B$ , because, after  $\theta_B$ ,  $\varepsilon_p^0 > \tan^2 \theta_B^2$ . Likewise,  $\varepsilon_p^1$  can be constant only when  $\theta$  varies between  $\theta_B$  and  $\theta_1$ , because, after  $\theta_1$ ,  $\varepsilon_p^1 > 2 \sin^2 \theta > \tan^2 \theta_B$ . On the other hand,  $\varepsilon_p^2$  can be constant for  $\theta$  between  $\theta_1$  and  $\frac{\pi}{2}$ , because  $\tan^2 \theta_B < \varepsilon_p^2 < 2 \sin^2 \theta$  (see Fig. 2).

The solutions  $\varepsilon_n$  and  $\varepsilon_p$  coincide on all of  $[0, \frac{\pi}{2}]$  if and only if the compatibility condition:

$$\lambda_n^2 \cos^2 \theta + \sin^2 \theta = \lambda_n \mu_p \quad (15)$$

holds in  $[0, \frac{\pi}{2}]$ , where, as in Eq. (7),

$$\lambda_n := \frac{1 + \gamma_n}{1 - \gamma_n} > 1, \quad (16)$$

together with the additional conditions  $\gamma_p \leq \gamma_n^2$ , if  $\theta_B \leq \theta \leq \theta_1$ , or  $\gamma_n^2 \leq \gamma_p$ , if  $\theta_1 \leq \theta < \frac{\pi}{2}$ . In this case, the common solution  $\varepsilon_n = \varepsilon_p =: \varepsilon_c$  is given by

$$\varepsilon_c = \lambda_n \mu_p, \quad (17)$$

and  $\varepsilon_c$  is constant on  $[0, \frac{\pi}{2}]$ ; in fact, as mentioned above,

$$\varepsilon_c = \tan^2 \theta_B. \quad (18)$$

We note that the only cases in which the identity  $\gamma_n^2 = \gamma_p$  can hold for some  $\tilde{\theta}$ , together with the compatibility condition (15), are:  $\tilde{\theta} = \frac{\pi}{4}$  if  $\tilde{\theta} \in [0, \theta_B[$ , or  $\tilde{\theta} = \theta_1$  (defined in Eq. (9)) if  $\tilde{\theta} \in [\theta_B, \frac{\pi}{2}]$ , in

which case  $\varepsilon = 2 \sin^2 \theta_1 = 2\lambda_n^2/(1 + \lambda_n^2)$ . More precisely, the case  $\theta = \frac{\pi}{4}$  and  $\gamma_n^2 = \gamma_p$  is exceptional, in that Equations (4) and (5) are identities in  $\varepsilon$ ; that is, *any*  $\varepsilon \in \mathbb{R}$  (in fact, any  $\varepsilon \in \mathbb{C}$ ) is a solution.

The reflected GPS signals are predominantly LH [5], especially for satellites with high elevation (angles greater than  $60^\circ$ ). Using the Subscript LR to represent the scattering when a satellite incident signal (right-hand polarized) is scattered by the surface and inverts the polarization to the left-hand, the reflection coefficient,  $\Gamma_{LR}$ , can be written as a linear combination of vertical and horizontal polarization [15]:

$$\Gamma_{LR} = \frac{1}{2}(\Gamma_n - \Gamma_p) \tag{19}$$

Note that:

$$\gamma_n = \frac{1}{2}(|\Gamma_n - \Gamma_p| + |\Gamma_n + \Gamma_p|) \tag{20}$$

$$\gamma_p = \frac{1}{2}||\Gamma_n - \Gamma_p| - |\Gamma_n + \Gamma_p|| \tag{21}$$

If  $\theta = 0^\circ$ , then  $\Gamma_n = -\Gamma_p$ , therefore:

$$\gamma_n = \frac{1}{2}|\Gamma_n - \Gamma_p| = |\Gamma_{LR}| \tag{22}$$

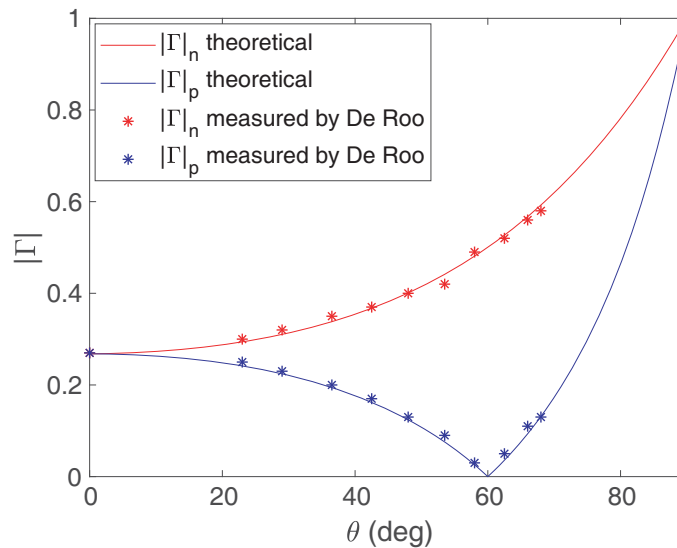
$$\gamma_p = \gamma_n \tag{23}$$

The values of signal to noise ratio (SNR) can be obtained from the GNSS-R measurements considering various satellites with different elevation angles. Considering the satellites with high elevation angles (i.e.,  $\theta \sim 0$ ), the SNR values the amplitude of the reflection coefficient  $|\Gamma_{LR}|$  can be obtained and the value of permittivity evaluated from 10.

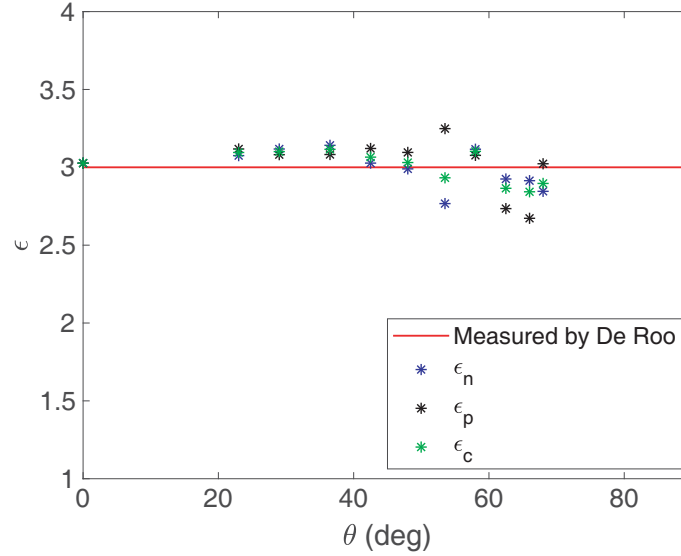
#### 4. RESULTS

As a first example, in Fig. 3 we consider the measurements of  $|\Gamma_n|$  and  $|\Gamma_p|$  reported in [18] for a medium composed of sand, for which  $\varepsilon = 3 + \sigma j$ , with  $|\sigma| \leq 0.05$ . We compute the values of  $\varepsilon_n$  and  $\varepsilon_p$  predicted by Eqs. (6) and (10), as well as the common value  $\varepsilon_c = \lambda_n \lambda_p$ .

We find that these values match the approximate value  $\varepsilon \approx 3$  with error not exceeding 1%. The measurements of  $|\Gamma_p|$  point to the evidence of a possible Brewster angle at approximately  $\theta_B = 60^\circ$  (which would be the exact value for  $\varepsilon = 3$ ). The relative error is given by  $e_c := \frac{1}{3}|\varepsilon_c - 3|$  (see Fig. 4).



**Figure 3.** Measurements of  $|\Gamma_n|$  and  $|\Gamma_p|$  reported in [18] (solid line) and data evaluated from (6) and (10) (dots).



**Figure 4.** Relative error.

As a second example, we consider some GNSS-R measurements carried out in a controlled environment located in Grugliasco, Torino (450358.5N, 73533.8E). In this location, a wide field of known characteristics (mainly 50% sand) belonging to the Interuniversity Department of Regional and Urban Studies and Planning (DIST), Politecnico di Torino, is available. The composition of the terrain is reported in Table 1. In this campaign, the direct GPS signals were measured using a right-hand circular polarized (RHCP) antenna, while the reflected signals were measured with a left-hand circular polarized (LHCP) antenna. The complete description of the setup can be found in [21]. In addition to the GNSS-R measurements, Time-Domain Reflectometry (TDR) measurements were carried out to be used as reference. An average value of about 6.4 was obtained for the permittivity. In Fig. 5, the magnitude of the two reflection coefficients is reported for  $\epsilon = 6.4$ . In particular, for a permittivity value equal to 6.4, for an elevation angle higher than  $80^\circ$  (corresponding to an incidence angle  $\theta$  less than  $20^\circ$ ), the difference between  $|\Gamma_n|$  and  $|\Gamma_p|$  is less than 0.043. In this case, the real permittivity can be obtained by using formula (10) for  $|\Gamma_p|$ .

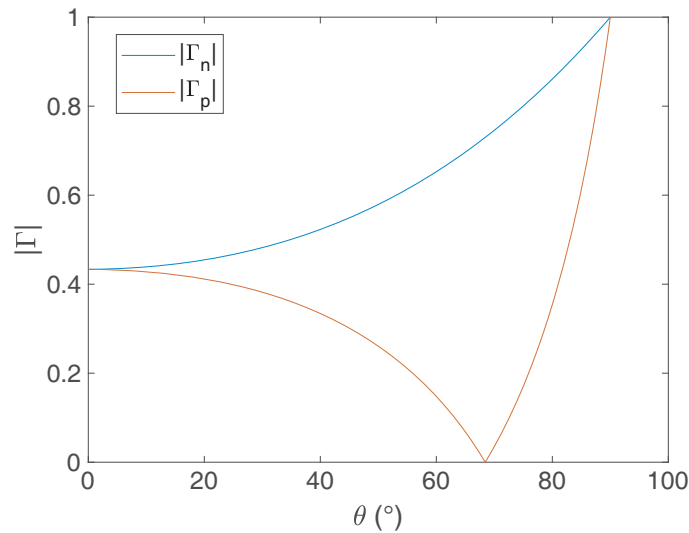
The results of the GNSS measurements and the computation of the permittivity values are reported in Table 2. Only satellite PRN 9 is considered because of its elevation. It can be observed that the values with an elevation angle greater than  $80^\circ$  are close to the results obtained with the TDR technique.

**Table 1.** Composition of the soil for the Grugliasco experiment.

Coarse sand (%)	Fine sand (%)	Very Fine sand (%)	
115.5	50.1	16.1	
Coarse silt (%)	Fine silt (%)	Clay (%)	Organic matter(%)
5.3	8.2	4.8	1.4

**Table 2.** Computation of the permittivity values from the measurements.

Elevation (deg)	$\theta$ (deg)	SNR (dB)	$ \Gamma_{LR} $	$\epsilon$
82.4	7.6	11	0.195	6.57
83.2	6.8	13	0.195	6.59



**Figure 5.** Amplitude of reflection coefficients for  $\epsilon = 6.4$ .

## 5. CONCLUSIONS

In GNSS-R for soil moisture applications, one essentially needs to determine the permittivity  $\epsilon$  of the soil from the Fresnel coefficients. For non-dispersive soil,  $\epsilon$  can be assumed real. In the literature,  $\epsilon$  is mostly found numerically. In fact, Equations (4) and (5) can be explicitly solved. We determine real solutions with  $\epsilon > 1$ , for all angles  $\theta \in [0, \frac{\pi}{2}[$  and all measurements  $\gamma_n, \gamma_p \in ]0, 1[$ , with  $\gamma_p \leq \gamma_n$ , which satisfy the compatibility conditions (15).

Our results suggest two possible strategies to determine the solution. The first hinges on being able to find a value  $\gamma_p \approx 0$  at a particular position  $\tilde{\theta}$ ; then,  $\tilde{\theta}$  is an approximation of the Brewster angle, and the approximate solution is simply  $\epsilon \approx \tan^2 \tilde{\theta}$ , as per Eq. (18). Otherwise, one can take any angle  $\theta$  in  $[0, \frac{\pi}{4}[$ , and verify that the corresponding measurements of  $\gamma_n$  and  $\gamma_p$  satisfy condition (15). If so, the solution is  $\epsilon = \lambda_n \lambda_p$ , as per Eq. (17).

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